*Computing 21*, 3 (June 1994), 301-315.

[14] P. T. Homer and R. D. Schlichting. Using Schooner to support distribution and heterogeneity in the Numerical Propulsion System Simulation project. *Concurrency—Practice and Experience 6*, 4 (June 1994) 271-287.

[15] A. A. Khokhar, V. K. Prasanna, M. E. Shaaban and C. Wang. Heterogeneous computing: Challenges and opportunities. *IEEE Computer 26*, 6 (June 1993), 18-27.

[16] Pratt & Whitney. The Pratt & Whitney PW4084 Engine. On-line html document. (http://www.utc.com/PW4000/fam112.html)

[17] J. A. Reed and A. A. Afjeh. Distributed and parallel programming in support of zooming in numerical propulsion system simulation, *OAI/OSC/NASA Symposium on Application of Parallel and Distributed Computing*, Columbus, Ohio. April 1994.

[18] J. A. Reed. Development of an Interactive Graphical Aircraft Propulsion System Simulator. Master of Science Thesis, University of Toledo, August 1993.

[19] T. J. Sullivan et al. Energy Efficient Engine: Fan Test Hardware Detailed Design Report. NASA CR-165148, 1983.

[20] Transportable Applications Environment Plus. Programmer's Manual, Version 5.2. Goddard Space Flight Center, National Aeronautics and Space Administration. December 1992.

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**References**

[1] Advanced Visual Systems Inc. *AVS Developer's Guide* (Release 4.0), Part number: 320-0013-02, Rev B, Advanced Visual Systems Inc., Waltham, MA, May 1992.

[2] Aviation Trade News. *The Avion Online Newspaper 83,* 4 (February 8, 1995). On-line html document (http://avion.db.erau.edu/avion/issues/spring95/issue4/aviationtrade.html).

[3] R. W. Bucy et al. Energy Efficient Engine: Component Development & Integration, Steady-State Performance Computer Program User's Manual for the IBM 370 and CDC 6600 Computers, GE Reference Computer Program - G0045I. R83AEB553, October, 1983.

[4] D. L. Burrus et al. Energy Efficient Engine: Combustor Test Hardware Detailed Design Report. NASA CR-168301, March 1984.

[5] R. W. Claus, A. L. Evans, G. J. Follen. Multidisciplinary propulsion simulation using NPSS. *4th AIAA/USAF/NASA/OAI Symposium on Multi-disciplinary Analysis and Optimization*, Cleveland, OH (September 1992).

[6] R. W. Claus, A. L. Evans, J. K. Lylte, and L. D. Nichols. Numerical propulsion system simulation. *Computing Systems in Engineering 2*, 4 (April 1991), 357-364.

[7] CLIPS Reference Manual, Basic Programming Guide. Software Technology Branch, Lyndon B. Johnson Space Center. CLIPS Version 5.1, September 10, 1991.

[8] D. Y. Davis and E. M. Stearns. Energy Efficient Engine—Flight Propulsion System Final Design and Analysis. NASA CR-168219, contract report prepared by General Electric Company, August 1985.

[9] GE 90, General Electric Aircraft Engines. On-line html document (http://www.ge.com/aircraftengines/ge90).

[10] E. J. Hall, R. A. Delaney, and J. L. Bettner. Investigation of Advanced Counterrotation Blade Configuration Concepts for High Speed Turboprop Systems, Task 5 — Unsteady Counterrotation Ducted Propfan Analysis Computer Program User's Manual, NASA CR-187125, Jan. 1993.

[11] R. Hayes. UTS: A Type System for Facilitating Data Communication. Ph.D. Dissertation, Department of Computer Science, University of Arizona, August 1989.

[12] P. R. Holloway et al. Energy Efficient Engine: High Pressure Compressor Detailed Design Report. NASA CR-165558, 1985.

[13] P. T. Homer and R. D. Schlichting. A software platform for constructing scientific applications from heterogeneous resources. *Journal of Parallel and Distributed*

| | TESS | Monitoring tool | ADPAC watch-dog |
|---|---|---|---|
| Development and testing | SGI 4D/480, or Sun Sparc10 NASA Lewis | Sun Sparc10 NASA Lewis Research Center | Nodes on a cluster of IBM RS-6000 workstations, or nodes on an IBM SP-2 NASA Lewis Research Center, Cleveland, OH |
| | SGI 4D/440 University of Toledo | Sun Sparc10 University of Arizona | |
| SC'94 Washington, D.C. | SGI Onyx Conference floor | Sun Sparc10 Conference floor | |
| SC'95 San Diego, Ca. | SGI Indy Conference floor | Sun Sparc10 Conference floor | |

**Table 1: Configurations used to test prototype simulation system**

areas. First, the expert system needs to detect and handle convergence problems that arise in the zooming strategy. For example, these include numerical inconsistencies between solvers used in the high- and low-fidelity simulations, and the ill-defined boundary condition problem described in Section 3.1. The second area is machine availability. This can range from dealing with short duration network outages to machine downtime schedules. For example, when a network outage occurs, the expert system may decide that enough ADPAC results are available to build the performance map, or that the simulation should wait until the network connection is restored, or that new ADPAC runs should be started on other accessible machines.

Another direction is to modify the source code of ADPAC to allow it to communicate directly with TESS and the monitoring and control system, rather than through its output files. A principal reason for not modifying the source initially is the desire to prove the feasibility of this approach and identify the specific changes needed. Another positive feature associated with using the output files is that it would be relatively straight-forward to substitute a different high-fidelity fan simulation and provide a similar level of monitoring through its output files. This technique allows for easy testing of different fan simulations without the initial need to involve the authors of the simulation.

Another zooming approach being studied is to use an intermediate fan simulation, specifically a two-dimensional, axisymmetric simulation. This has the advantage of not requiring as much execution time as the three-dimensional ADPAC simulation when less accuracy is needed. In addition, it will be possible in some cases to use the solution from the medium-fidelity simulation to jump-start the three-dimensional solution, thus shortening the execution time of the high-fidelity simulation.

The Schooner system is being extended to include better fault detection techniques and provide information about failures to the expert system and to the user. Schooner is also being extended to work with batch queueing systems which will provide greater access to machine resources. This will facilitate longer simulation runs by providing ADPAC platforms during more hours each day.

module. The configuration shown in Figure 4 is for the $E^3$ engine. Steady-state overall performance maps for the operation of the fan, high-pressure compressor, high-pressure turbine, and low-pressure turbine were constructed from engine design and test-stand data [3, 4, 12, 19]. Individual component design-point data, based on design and cycle-deck data, are used to define the operational parameters in each component. The TESS $E^3$ engine model can be executed in both zooming and non-zooming modes; the choice is made by selecting the appropriate fan component. Figure 4 shows the zooming mode with the *fan Multi-ADPAC* module in the engine.

### 5.2 High-fidelity fan

A grid geometry model representing the engine cowl, fan, bypass, and S-duct regions was developed from the $E^3$ fan geometry data. An axisymmetric view of the grid is shown in Figure 10b. Booster rotor and stator, core outlet guide vanes, and bypass outlet guide vane geometry were not included in order to reduce computing times. Experience modeling the $E^3$ fan with complete geometry has shown that computing time increases by approximately a factor of four when these components are included. For this work, overall simulation time is highly dependent on the ADPAC simulations; the increased time of computation outweighs the marginal improvement in predicted values when the additional geometry is included. The structured, multi-blocked, three-dimensional grid represents a single blade passage and consists of 16,380 grid points. The steady flow field in the fan is analyzed using the ADPAC solver and the given geometry to solve the inviscid Euler equations. To determine the single-valued flow parameters for the exit boundary condition, the mass-averaging process is applied at a location approximately one and one-half fan diameters downstream of the fan trailing-edge.

### 5.3 System Configuration

The prototype simulation system has been tested in several configurations. The following list shows the platforms that each part of the system can currently use:

- TESS executes within AVS version 5, and has been tested on SGI and Sun architectures,
- The Monitoring tool uses TAE+ version 5.2 and has been tested on Sun workstations, and
- The ADPAC binaries available for this project are compiled for the IBM RS-6000 and SP-2 architectures.

An early version of the system was demonstrated at Supercomputing ‘94 and the current version was demonstrated at Supercomputing ‘95. Table 1 summarizes these configurations and two development versions that are in use for testing zooming strategies and expert system techniques.

## 6. Future Work

The prototype simulation system described here provides a framework for developing and evaluating new zooming strategies, implementing monitoring and control system techniques, and addressing interconnection and configuration problems. The major need in the prototype is for expansion of the role of the expert system to allow long unsupervised simulation runs. The system as it currently exists has been tested and works well for simulation runs of up to several hours. To achieve longer, more realistic simulation runs requires expert system assistance in two broad